# Example 5: Immediate settlement under a circular tank on layered subsoil

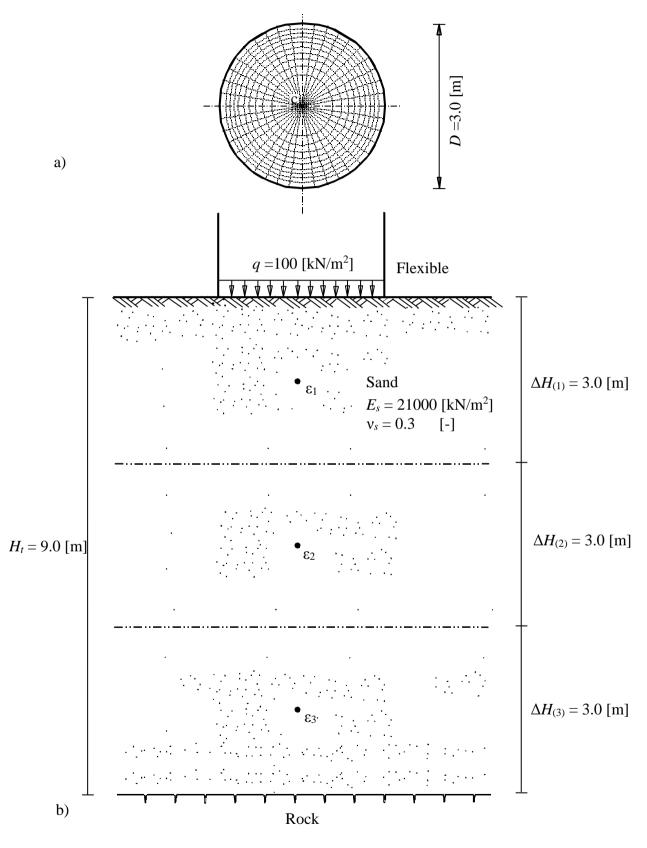
## **1** Description of the problem

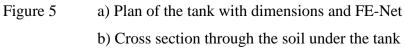
To verify the immediate settlement under a circular loaded area calculated by *ELPLA*, the immediate settlement at the center of a tank calculated by *Das* (1983), Example 6.2, page 354, is compared with that obtained by *ELPLA*.

A circular tank of 3.0 [m] diameter is considered as shown in Figure 5. The base of the tank is assumed to be flexible and having a uniform contact pressure of  $q = 100 \text{ [kN/m^2]}$ . A sand layer 9.0 [m] thick is located under the tank. The modulus of elasticity of the sand is  $E_s = 21000 \text{ [kN/m^2]}$  while *Poisson's* ratio of the sand is  $v_s = 0.3$  [-]. It is required to determine the immediate settlement at the center of the tank for two cases:

- Considering the underlying soil as one layer of 9.0 [m] thickness
- Dividing the underlying soil into three layers of equal thickness of 3.0 [m]

## Examples to verify and illustrate ELPLA





#### 2 Hand calculation of the immediate settlement

According to *Das* (1983), the immediate settlement at the center of the tank can be obtained by hand calculation as follows:

a) Considering the underlying soil as one layer of 9.0 [m] thickness

The vertical deflection  $s_e$  [m] under the center of a circular loaded area at a depth z [m] from the surface can be obtained from

$$s_{e} = q \frac{1 + ny_{s}}{E_{s}} r \left[ \frac{z}{r} I_{1} + (1 - ny_{s}) I_{2} \right]$$
(6)

where:

- $I_1, I_2$  Coefficients for vertical deflection (which is a function of z/r and s/r) according to *Ahlvin/Ulery* (1962) [-]
- $v_s$  Poisson's ratio of the soil [-]
- $E_s$  Modulus of elasticity of the soil [kN/m<sup>2</sup>]
- *r* Radius of the circular area [m]
- q Load intensity [kN/m<sup>2</sup>]
- *s* Distance from the center of the circular area [m]

### Settlement at the surface $s_{e(z=0)}$

At surface z/r = 0 and s/r = 0. Then,  $I_1 = 1$  and  $I_2 = 2$ 

$$s_{e(z=0)} = 100 \frac{1+0.3}{21000} 1.5 [0+(1-0.3)2] = 0.013 [m]$$

### Settlement at depth z = 9.0 [m] from the surface $s_{e(z=9)}$

For z/r = 9/1.5 = 6 and s/r = 0. Then,  $I_1 = 0.01361$  and  $I_2 = 0.16554$ 

$$s_{e(z=9)} = 100 \frac{1+0.3}{21000} 1.5 \left[\frac{9}{1.5} 0.0136 + (1-0.3)0.16554\right] = 0.00183 [m]$$

The immediate settlement  $s_e$  is given by

$$s_e = s_{e(z=0)} - s_{e(z=9)} = 0.0130 - 0.00183 = 0.01117$$
 [m]

Examples to verify and illustrate ELPLA

b) Dividing the underlying soil into three layers of equal thickness of 3.0 [m]

Another general method for estimation of immediate settlement is to divide the underlying soil into *n* layers of finite thickness  $\Delta H_{(i)}$ . If the strain  $\varepsilon_{z(i)}$  at the middle of each layer can be calculated, the total immediate settlement  $s_e$  [m] can be obtained as

$$s_e = \sum_{i=1}^{i=n} \Delta H_{(i)} \epsilon_{z(1)}$$
(7)

The strain  $\varepsilon_z$  at the middle of the layer is given by

$$\varepsilon_{z} = q \frac{1 + ny_{s}}{E_{s}} \left[ \left( 1 - 2ny_{s} \right) A^{\dagger} + B^{\dagger} \right]$$
(8)

where:

A', B' Coefficients for vertical deflection (which is a function of z/r and s/r) according to *Ahlvin/Ulery* (1962)

### Layer (1)

For z/r = 1.5/1.5 = 1 and s/r = 0. Then, A' = 0.29289 and B' = 0.35355

#### Layer (2)

For z/r = 4.5/1.5 = 3 and s/r = 0. Then, A' = 0.05132 and B' = 0.09487

#### Layer (3)

For z/r = 7.5/1.5 = 5 and s/r = 0. Then, A' = 0.01942 and B' = 0.03772

The final stages in the calculation are listed in Table 5.

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| Layer<br>No. | Layer thickness $\Delta H_{(i)}$ [m] | Strain at the center of the layer $\varepsilon_{z(i)}$ [-] | Immediate settlement $s_{e(i)}$ [m] |
|--------------|--------------------------------------|--|-------------------------------------|
| 1            | 3.0                                  | 0.00291  | 0.00873                             |
| 2            | 3.0                                  | 0.00071  | 0.00213                             |
| 3            | 3.0                                  | 0.00028  | 0.00084                             |
|              | Total immediate                      | 0.0117   |                                     |

Table 5 Final stages in the calculation of immediate settlement  $s_e$ 

### 3 Immediate settlement by *ELPLA*

The tank rests on a layer of sand. However, in *ELPLA*, it will be sufficiently accurate to consider the sand layer as a whole but the immediate settlement is to be calculated twice. The first calculation by considering the underlying soil as one layer of 9.0 [m] thickness and the second calculation by dividing the underlying soil into three layers of equal thickness of 3.0 [m]. The contact pressure of the tank in this example is known where the tank base is considered to be flexible. Therefore, the available method "Flexible foundation 9" in *ELPLA* is used here to determine the immediate settlement of the sand layer. The immediate settlements obtained by *ELPLA* under the center of the tank in both cases of calculations are compared with those obtained by hand calculation in Table 6.

| Table 6 | Comparison of immedi | ate settlements $s_e$ [cm] | ] obtained by ELPLA and | Das (1983) |
|---------|----------------------|----------------------------|-------------------------|------------|
|---------|----------------------|----------------------------|-------------------------|------------|

|  | <i>s</i> <sub>e</sub> [cm] |       |  |
|--|----------------------------|-------|--|
| Calculation                                    | Das (1983)                 | ELPLA |  |
| Considering the underlying soil as one layer   | 1.117                      | 1.115 |  |
| Dividing the underlying soil into three layers | 1.170                      | 1.115 |  |

Table 6 shows that results of the immediate settlements obtained by *ELPLA* and those obtained by *Das* (1983) for both cases are in good agreement.